# $\mathrm{M}_{\mathrm{w}}$ Estimation for Regional Seismic Events in the Friuli Area (NE Italy) 

Department of Earth Sciences, University of Trieste, Italy


## The rationale behind this work

- Within an Interreg IIIb Project between Austria and Italy, with the support from Slovenia, a real-time transfrontier network of seismic stations (broadband, strong motion) has been implemented at the contact AlpsDinarides and runs with the BRTT Antelope ${ }^{\ominus}$ system.
- The need for an independent estimate of magnitude has arisen, since the single national and regional networks each use a different magnitude (different local, duration, coda etc.) and there is no moment estimate for events with magnitude $<5$ from transnational agencies. This is also a task of the Project ProCiv-INGV 2004-06: S4.
- By estimating in real time the moment magnitude for the events recorded by the network, all events could have a common independent parameter, that would also allow and easier comparison with events from other regions.

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## Method used to determine the seismic mo

(Andrews 1986)

Spectral amplitude at receiver

$$
A(f)=D(f) E(f) G(R)
$$

Brune (1970) Source Spectrum
$D(f)=\frac{M_{0}}{4 \pi k \rho v^{3}}\left[1+\left(\frac{f}{f_{0}}\right)^{2}\right]^{-1}$

$$
S V 2=2 \int_{0}^{\infty} V^{2}(f) d f
$$

$$
S V 2=\frac{1}{4} \Omega^{2}\left(2 \pi f_{0}\right)^{3}
$$

Attenuation

$$
E(f)=e^{-\left(\frac{\pi \pi f}{Q(f)}\right)}
$$

$$
G(R)=\frac{1}{R}
$$

$$
S D 2=2 \int_{0}^{\infty} D^{2}(f) d f
$$

$$
S D 2=\frac{1}{4} \Omega^{2}\left(2 \pi f_{0}\right)
$$

## Method (cont’d)

$$
\begin{aligned}
& S V 2=\frac{1}{4} \Omega^{2}\left(2 \pi f_{0}\right)^{3} \\
& S D 2=\frac{1}{4} \Omega^{2}\left(2 \pi f_{0}\right)
\end{aligned}
$$

$$
\Omega=\sqrt{4(S D 2)^{3 / 2}(S V 2)^{-1 / 2}}
$$

$$
f_{0}=\frac{1}{2 \pi} \sqrt{\frac{S V 2}{S D 2}}
$$

## $M_{0}=4 \pi \rho v^{3} \Omega k$

$$
M_{w}=\frac{2}{3} \cdot \log _{10}\left(M_{0}\right)-6,1
$$

$$
r=\frac{2.34 \beta}{2 \pi f_{0}}
$$

The signal and the instrument response are extracted from the database of the Antelope ${ }^{\odot}$ system at DST

Average and instrument response are removed and bandpass filter applied


EW and NS components are combined to obtain the trasversal one to minimize P-wave interferences
"noise" window and "S" window are retrieved and sinusoidal tapering at edges applied

## Extracted noise

Extracted S-wave signal



Signal-to-Noise spectral ratio is used to determine the frequency window


Requirements
at least a point with $\mathrm{S} / \mathrm{R}>2.5$

$$
\begin{gathered}
S / R>2.5 \text { for } f_{\text {inf }} \\
S / R>5.0 \text { for } f_{\text {sup }} \\
f_{\text {sup }}<10 H z
\end{gathered}
$$

If the requirements are not met an error message is printed and the signal is rejected

From the signals in acceleration or velocity

Integrate to obtain velocities and displacements
-FFT
-Correction for geometrical spreading and anelastic attenuation


$$
\sqrt{5}
$$

Velocity and displacement spectra estimated
AT THE SOURCE

## Example of Estimated Source Spectrum and Theoretical Fit



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## Constraints

$$
f_{0}>2 \cdot f_{\mathrm{inf}} \quad f_{0}<f_{\text {sup }}
$$

$$
1 \cdot 10^{4} \mathrm{~Pa}<\Delta \sigma<1 \cdot 10^{8} \mathrm{~Pa}
$$

where

$$
\Delta \sigma=\frac{7 M_{0}}{16}\left(\frac{2 \pi f_{0}}{2,34 \beta}\right)^{3}
$$

If these constraints are NOT met an message is printed and the signal rejected

NOTE: These constraints are still being tested!

## Example of computed table

| Message | Station | Channel | Type | f inf | f sup | f0 | M0 | Mw | Distance | Azimuth |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OK | MOGG | HG | A | 0.1 | 9.9 | 1.2 | $1.42 \mathrm{E}+16$ | 4.7 | 35,154 | 106 |
| OK | GEPF | HG | A | 0.1 | 9.9 | 0.6 | $5.90 \mathrm{E}+16$ | 5.1 | 37,849 | 83 |
| OK | CESC | HG | A | 0.1 | 9.9 | 0.2 | $2.97 \mathrm{E}+17$ | 5.6 | 44,068 | 95 |
| att.,stress drop" | STOL | HG | A | 0.1 | 9.8 | 1.1 | $3.74 \mathrm{E}+16$ | 5.0 | 21,748 | 102 |
| OK | MASA | HG | A | 0.1 | 9.9 | 0.5 | $1.07 \mathrm{E}+17$ | 5.3 | 21,914 | 45 |
| OK | PRAD | HG | A | 0.1 | 10.0 | 0.4 | $4.31 \mathrm{E}+16$ | 5.0 | 57,238 | 82 |
| Sup min inf | CARC | HG | A | 0.0 | 0.0 | 0.0 | $0.00 \mathrm{E}+00$ | 0.0 | 73,941 | 352 |
| OK | LJU | HG | A | 0.0 | 10.0 | 0.4 | $1.99 \mathrm{E}+17$ | 5.4 | 74,376 | 294 |
| OK | MAJA | HG | A | 0.1 | 9.9 | 0.4 | $6.96 \mathrm{E}+16$ | 5.1 | 45,585 | 71 |
| OK | OBKA | HH | V | 0.0 | 10.0 | 0.3 | $1.60 \mathrm{E}+17$ | 5.4 | 72,374 | 253 |
| OK | CADS | HH | V | 0.2 | 9.8 | 1.1 | $2.55 \mathrm{E}+16$ | 4.8 | 12,618 | 322 |
| OK | TRI | HH | V | 0.0 | 10.0 | 0.6 | $2.64 \mathrm{E}+16$ | 4.9 | 67,750 | 352 |
| OK | KNDS | HH | V | 0.0 | 10.0 | 0.4 | $1.06 \mathrm{E}+17$ | 5.3 | 103,812 | 327 |
| OK | CEY | HH | V | 0.0 | 10.0 | 0.5 | $6.64 \mathrm{E}+16$ | 5.1 | 87,657 | 317 |
| OK | CRES | HH | V | 0.0 | 9.5 | 0.4 | $1.18 \mathrm{E}+17$ | 5.3 | 149,148 | 292 |
| OK | ARSA | HH | V | 0.0 | 10.0 | 0.2 | $2.00 \mathrm{E}+17$ | 5.4 | 175,230 | 235 |
| OK | KBA | HH | V | 0.0 | 10.0 | 0.5 | $2.46 \mathrm{E}+16$ | 4.8 | 86,367 | 165 |
| OK | DST2 | HH | V | 0.0 | 9.9 | 0.6 | $3.52 \mathrm{E}+16$ | 4.9 | 73,662 | 350 |
| OK | VINO | BH | V | 0.1 | 9.9 | 1.1 | $1.58 \mathrm{E}+16$ | 4.7 | 27,772 | 76 |
| Average values |  |  |  |  |  | $0.6 \pm 0.3$ |  | $5.1 \pm 0.3$ |  |  |

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Dismiss
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latency 30.0 \# group latency
maxwaittime 60.0 \# A hard timeout value in seconds for reading waveform packets.
\# If no waveform packets for the selected channels are received
\# within this time period, then the waveform reading loop is
\# interrupted and any further processing for that event is
\# aborted.
v_r 4.0 \# velocity for surface waves used to determine surface wave arrival time
auto_arr no \# start of measuring time window yes = computed arrival
no $=\mathrm{db}$ arrival
time_window_factor
1.0 \# The waveform for processing the magnitude is determined by a time \# window starting from the arrival defined by the time0 parameter \# to time_factor*(S_time-P-time) seconds after the first P-arrival.

```
distmin 0 # distance range in km
distmax 200 #
```

q 800 \# attenuation value
\# the M0 formula implemented is: $\mathrm{M} 0=4 * \mathrm{pi}^{*} \mathrm{OMEGA}^{*} \mathrm{c} 1^{*} \mathrm{c} 2 \wedge 3 * \mathrm{c} 3$
c1 0.63 \# avarage directivity
c2 3400 \# velocity S wave m/s
c3 2700 \# average density
\# the MW formula implemented is: $\mathrm{MW}=\mathrm{c} 4 * \log 10(\mathrm{M} 0)-\mathrm{c5}$
c4 0.667
c5 6.1
filter BW 0.055105
mag \&Tbl \{
\# stations parameters for computing magnitudes
\# calib deconvolve apply snr twin
\#sta expr db response filter thresh noise c2 c3 c4 c5 minclip maxclip
ARSA HH yes no no $\begin{array}{llllllllllllll}2.0 & 60.0 & 0.0 & 0.0 & 1.0 & 1.0 & 0.0\end{array}$
CEY HH yes no no $\begin{array}{llllllllll}2.0 & 60.0 & 0.0 & 0.0 & 1.0 & 1.0 & 0.0\end{array}$


Origin time: 23 February 2007 06:14:39.419 Lat. 47.011 Lon. $13.270 \mathrm{Ml}=3.11$
ACOM chan: HH Distance: 5.410785e+01 Az: 3.402557e+02 P 06:14:48.658 db S 06:14:55.704 synt noise window start: 06:14:28.622 stop: 06:14:46.658
S window start: 06:14:54.780 stop: 06:15:13.740
signal window start: 06:14:28.622 stop: 06:15:15.740
arrP $1.172211289 \mathrm{e}+09$ otime $1.172211279 \mathrm{e}+09$ trtime $1.628496170 \mathrm{e}+01$
$\mathrm{Mw}=2.56 \mathrm{M} 0=9.47 \mathrm{e}+12 \mathrm{f0}=5.78 \mathrm{OK}$ stype $=\mathrm{V}$ delfrq $=0.0528 \mathrm{fmin}=0.5277 \mathrm{fmax}=9.9736$
AQU chan: HH Distance: 512.16 out of limits ( $0.00,200.00$ )
ARSA chan: HH Distance: 1.706005e+02 Az: 2.619437e+02 P 06:15:07.996 db S 06:15:30.764 synt noise window start: 06:14:09.129 stop: 06:15:05.996
S window start: 06:15:27.906 stop: 06:16:27.631
signal window start: 06:14:09.129 stop: 06:16:29.631
arrP $1.172211308 \mathrm{e}+09$ otime $1.172211279 \mathrm{e}+09$ trtime $5.134459305 \mathrm{e}+01$
$\mathrm{Mw}=2.49 \mathrm{M} 0=7.58 \mathrm{e}+12 \mathrm{f0}=3.84 \mathrm{OK}$ stype $=\mathrm{V}$ delfrq $=0.0167 \mathrm{fmin}=0.6364 \mathrm{fmax}=9.9812$
CADS chan: HH Distance: $9.301553 \mathrm{e}+01 \mathrm{Az}: 3.378922 \mathrm{e}+02$ P $06: 14: 55.139 \mathrm{db} \mathrm{S} 06: 15: 07.414$ synt noise window start: 06:14:22.134 stop: 06:14:53.139
S window start: 06:15:05.842 stop: 06:15:38.419
signal window start: 06:14:22.134 stop: 06:15:40.419
$\operatorname{arrP} 1.172211295 \mathrm{e}+09$ otime $1.172211279 \mathrm{e}+09$ trtime $2.799492645 \mathrm{e}+01$
$\mathrm{Mw}=2.62 \mathrm{M} 0=1.18 \mathrm{e}+13 \mathrm{f} 0=5.55 \mathrm{OK}$ stype $=\mathrm{V}$ delfrq= $0.0307 \mathrm{fmin}=1.1972 \mathrm{fmax}=9.9770$
CEY chan: HH Distance: 1.650012e+02 Az: 3.284280e+02 P 06:15:07.777 db S 06:15:29.079 synt noise window start: 06:14:10.776 stop: 06:15:05.777
S window start: 06:15:26.243 stop: 06:16:24.079
signal window start: 06:14:10.776 stop: 06:16:26.079 $\operatorname{arrP} 1.172211308 \mathrm{e}+09$ otime $1.172211279 \mathrm{e}+09$ trime $4.965950775 \mathrm{e}+01$

Station rejected:
no freqmax found!
CRES chan: HH Distance: 210.83 out of limits $(0.00,200.00)$
DOBS chan: HH Distance: $1.913175 \mathrm{e}+02 \mathrm{Az}: 3.004683 \mathrm{e}+02 \mathrm{P} 06: 15: 12.776$ synt $\mathrm{S} 06: 15: 36.999$ synt
noise window start: 06:14:07.003 stop: 06:15:10.776
S window start: 06:15:33.663 stop: 06:16:40.771
signal window start: 06:14:07.003 stop: 06:16:42.771
$\operatorname{arrP} 1.172211313 \mathrm{e}+09$ otime $1.172211279 \mathrm{e}+09$ trtime $5.757920837 \mathrm{e}+01$
Station rejected: $\quad$ freqmax $<$ freqmin after $Q$ correction

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## Processed Events

(3 major ones (Ml>4.5) and 193 minor ones) Preliminary Antelop locations on large grids is shown


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## BOVEC



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## RISULTATI MANUALI

| Messaggio | stazione | canale | Tipo | finf | f sup | f0 | M0 | Mw | distanza | Azimut |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OK | MOGG | HG | A | 0.1 | 9.9 | 0.3 | $1.22 \mathrm{E}+17$ | 5.3 | 35,154 | 106 |
| OK | GEPF | HG | A | 0.1 | 9.9 | 0.6 | $4.97 \mathrm{E}+16$ | 5.0 | 37,849 | 83 |
| OK | CESC | HG | A | 0.1 | 9.9 | 0.3 | $1.56 \mathrm{E}+17$ | 5.4 | 44,068 | 95 |
| att.,Sd"sospetto" | STOL | HG | A | 0.1 | 9.8 | 1.2 | $3.58 \mathrm{E}+16$ | 4.9 | 21,748 | 102 |
| OK | MASA | HG | A | 0.1 | 9.9 | 0.4 | $1.79 \mathrm{E}+17$ | 5.4 | 21,914 | 45 |
| OK | PRAD | HG | A | 0.1 | 10.0 | 0.3 | $5.73 \mathrm{E}+16$ | 5.1 | 57,238 | 82 |
| OK | CARC | HG | A | 0.0 | 9.9 | 0.7 | $5.50 \mathrm{E}+16$ | 5.1 | 73,941 | 352 |
| OK | LJU | HG | A | 0.0 | 10.0 | 0.6 | $1.27 \mathrm{E}+17$ | 5.3 | 74,376 | 294 |
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| OK | OBKA | HH | V | 0.0 | 10.0 | 0.3 | $1.57 \mathrm{E}+17$ | 5.4 | 72,374 | 253 |
| OK | CADS | HH | V | 0.2 | 9.8 | 1.0 | $3.21 \mathrm{E}+16$ | 4.9 | 12,618 | 322 |
| OK | TRI | HH | V | 0.0 | 10.0 | 0.6 | $2.54 \mathrm{E}+16$ | 4.8 | 67,750 | 352 |
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| OK | CRES | HH | V | 0.0 | 10.0 | 0.5 | $9.48 \mathrm{E}+16$ | 5.2 | 149,148 | 292 |
| OK | ARSA | HH | V | 0.0 | 10.0 | 0.3 | $1.21 \mathrm{E}+17$ | 5.3 | 175,230 | 235 |
| OK | KBA | HH | V | 0.0 | 10.0 | 0.5 | $2.41 \mathrm{E}+16$ | 4.8 | 86,367 | 165 |
| OK | DST2 | HH | V | 0.0 | 10.0 | 0.6 | $4.09 \mathrm{E}+16$ | 5.0 | 73,662 | 350 |
| OK | VINO | BH | V | 0.1 | 9.9 | 1.1 | $1.45 \mathrm{E}+16$ | 4.7 | 27,772 | 76 |
| Valori medi |  |  |  |  |  | $0.5 \pm 0.3$ | $8.35 \mathrm{E}+16$ | $5.1 \pm 0.2$ |  |  |

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RISULTATI AUTOMATICI

| Messaggio | stazione | canale | Tipo | finf | f sup | f0 | M0 | Mw | distanza | Azimut |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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| OK | CESC | HG | A | 0.1 | 9.9 | 0.2 | $2.97 \mathrm{E}+17$ | 5.6 | 44,068 | 95 |
| att.,sd"sospetto" | STOL | HG | A | 0.1 | 9.8 | 1.1 | $3.74 \mathrm{E}+16$ | 5.0 | 21,748 | 102 |
| OK | MASA | HG | A | 0.1 | 9.9 | 0.5 | $1.07 \mathrm{E}+17$ | 5.3 | 21,914 | 45 |
| OK | PRAD | HG | A | 0.1 | 10.0 | 0.4 | $4.31 \mathrm{E}+16$ | 5.0 | 57,238 | 82 |
| sup min inf | CARC | HG | A | 0.0 | 0.0 | 0.0 | $0.00 \mathrm{E}+00$ | 0.0 | 73,941 | 352 |
| OK | LJU | HG | A | 0.0 | 10.0 | 0.4 | $1.99 \mathrm{E}+17$ | 5.4 | 74,376 | 294 |
| OK | MAJA | HG | A | 0.1 | 9.9 | 0.4 | $6.96 \mathrm{E}+16$ | 5.1 | 45,585 | 71 |
| OK | OBKA | HH | V | 0.0 | 10.0 | 0.3 | $1.60 \mathrm{E}+17$ | 5.4 | 72,374 | 253 |
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| OK | TRI | HH | V | 0.0 | 10.0 | 0.6 | $2.64 \mathrm{E}+16$ | 4.9 | 67,750 | 352 |
| OK | KNDS | HH | V | 0.0 | 10.0 | 0.4 | $1.06 \mathrm{E}+17$ | 5.3 | 103,812 | 327 |
| OK | CEY | HH | V | 0.0 | 10.0 | 0.5 | $6.64 \mathrm{E}+16$ | 5.1 | 87,657 | 317 |
| OK | CRES | HH | V | 0.0 | 9.5 | 0.4 | $1.18 \mathrm{E}+17$ | 5.3 | 149,148 | 292 |
| OK | ARSA | HH | V | 0.0 | 10.0 | 0.2 | $2.00 \mathrm{E}+17$ | 5.4 | 175,230 | 235 |
| OK | KBA | HH | V | 0.0 | 10.0 | 0.5 | $2.46 \mathrm{E}+16$ | 4.8 | 86,367 | 165 |
| OK | DST2 | HH | V | 0.0 | 9.9 | 0.6 | $3.52 \mathrm{E}+16$ | 4.9 | 73,662 | 350 |
| OK | VINO | BH | V | 0.1 | 9.9 | 1.1 | $1.58 \mathrm{E}+16$ | 4.7 | 27,772 | 76 |

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Comparison between "manual" and "automatic" results

Bovec '04


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## $\mathrm{M}_{\mathrm{W}}$ as a function of distance

No station corrections applied for these tests

Bovec '04


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## Carnia 2004




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RISULTATI MANUALI

| Messaggio | stazione | Canale | tipo | finf | fsup | f0 | M0 | Mw | distanza | Azimut |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OK | PRAD | HG | A | 0.1 | 9.9 | 0.6 | $8.18 \mathrm{E}+15$ | 4.5 | 25,735 | 55 |
| OK | MOGG | HG | A | 1.0 | 8.6 | 2.4 | $1.12 \mathrm{E}+15$ | 3.9 | 3,161 | 217 |
| OK | GEPF | HG | A | 0.3 | 9.7 | 0.7 | $5.33 \mathrm{E}+15$ | 4.4 | 11,738 | 9 |
| OK | STOL | HG | A | 0.2 | 9.8 | 0.6 | $9.59 \mathrm{E}+16$ | 5.2 | 14,656 | 280 |
| OK | GESC | HG | A | 0.3 | 9.6 | 0.6 | $3.37 \mathrm{E}+16$ | 4.9 | 11,218 | 9 |
| OK | MASA | HG | A | 0.1 | 9.9 | 1.0 | $1.03 \mathrm{E}+16$ | 4.6 | 30,446 | 318 |
| OK | KBA | HH | V | 0.0 | 10.0 | 2.1 | $4.50 \mathrm{E}+15$ | 4.3 | 77,698 | 190 |
| OK | ARSA | HH | V | 0.0 | 10.0 | 0.6 | $1.48 \mathrm{E}+16$ | 4.7 | 201,522 | 243 |
| OK | OBKA | HH | V | 0.0 | 10.0 | 1.4 | $8.11 \mathrm{E}+15$ | 4.5 | 105,834 | 263 |
| OK | MOA | HH | V | 0.0 | 10.0 | 1.2 | $1.21 \mathrm{E}+16$ | 4.6 | 181,128 |  |
| OK | VINO | BH | V | 0.2 | 9.2 | 1.2 | $2.54 \mathrm{E}+15$ | 4.2 | 16,519 |  |
| Valori medi |  |  |  |  | $1.1 \pm 0.6$ | $1.79 \mathrm{E}+16$ | $4.5 \pm 0.3$ |  | 328 |  |


|  |  | RISULTATI AUTOMATICI |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| messaggio | staz | canale | tipo | finf | f sup | f0 | M0 | Mw | dist | azimut |
| OK | PRAD | HG | A | 0.1 | 9.9 | 2.5 | $9.84 \mathrm{E}+14$ | 3.9 | 25,735 |  |
| f0sulliminf | MOGG | HG | A | 1.0 | 8.6 | 1.6 | $2.72 \mathrm{E}+14$ | 3.5 | 3,161 |  |
| OK | GEPF | HG | A | 0.3 | 9.7 | 0.8 | $3.42 \mathrm{E}+15$ | 4.3 | 11,738 | 217 |
| att,sd"sospetto" | STOL | HG | A | 0.2 | 9.8 | 1.4 | $2.94 \mathrm{E}+16$ | 4.9 | 14,656 | 280 |
| OK | GESC | HG | A | 0.3 | 9.6 | 0.5 | $3.10 \mathrm{E}+16$ | 4.9 | 11,218 | 9 |
| OK | MASA | HG | A | 0.1 | 9.9 | 1.5 | $5.43 \mathrm{E}+15$ | 4.4 | 30,446 | 318 |
| OK | KBA | HH | V | 0.0 | 10.0 | 1.3 | $4.88 \mathrm{E}+15$ | 4.4 | 77,698 |  |
| OK | ARSA | HH | V | 0.0 | 10.0 | 0.5 | $1.94 \mathrm{E}+16$ | 4.8 | 201,522 |  |
| OK | OBKA | HH | V | 0.0 | 10.0 | 1.3 | $1.03 \mathrm{E}+16$ | 4.6 | 105,834 |  |
| OK | MOA | HH | V | 0.0 | 10.0 | 1.1 | $1.40 \mathrm{E}+16$ | 4.7 | 181,128 |  |
| OK | VINO | BH | V | 0.2 | 9.9 | 1.3 | $2.29 \mathrm{E}+15$ | 4.2 | 16,519 |  |
| valori medi |  |  |  |  |  | $1.3 \pm 0.6$ | $1.10 \mathrm{E}+16$ | $4.4 \pm 0.4$ | 207 |  |

## Site Effects

STOL (Stolvizza) e GESC (Gemona Scugelars)
Stations used to study site effects


## Comparison with $\mathrm{M}_{\mathrm{L}}\left(\right.$ Antelope $\left.^{\ominus}\right)$

Small Events (193 events 3576 traces) ( $\sim 18$ stations/event)


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Single-station deviations with respect to average as a function of distance (trace by trace, with 1787 traces successfully processed $\sim 50 \%$ of total )

$$
s(d)=M_{W}(d)-\overline{M_{W}}
$$



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| $\pm 0.2$ | $60.0 \%$ |
| :--- | :--- |
| $\pm 0.3$ | $77.5 \%$ |
| $\pm 0.5$ | $91.5 \%$ |
| $\pm 1.1$ | $98.5 \%$ |

The bias towards positive values could be explained with site effects at some stations

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Corner Frequency $\left(\mathrm{f}_{0}\right)$
High dispersion (Di Bona-Rovelli, 1988)

Equivalent radius (r)

$$
r=\frac{2.34 \beta}{2 \pi f_{0}}
$$



For the Bovec 1998 event: $S=4^{2} \pi \sim 50 \mathrm{~km}^{2}$
Bajc et al. (2001): 10kmx6km~60km²
(Inversion result)
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## Conclusions

-The method has given moment magnitude values in very good agreement with independent estimates for those events that have it.
-For all events the retrieved moment magnitudes are compatible, even for the smallest considered ones, with the local magnitudes given by the Antelope ${ }^{\oplus}$ system.
-The standard deviation of the single station moment magnitude estimates with respect to the average event estimate is rather low and does not depend on distance.
-For the Bovec 1998 event, for which there is an independent fault size estimate, the equivalent radius value derived with this method validates our procedure.
-Some ( $\sim 20$ ) events seem to have an anomalous equivalent radius, pointing to an either anomalously low stress drop or to possible unreliable corner frequency determination (reasons to be assessed, work in progress).
-The procedure is ready to be used in real-time on the Antelope ${ }^{\circledR}$ system.
AUG, Trieste - February 27-28, 2007

